

... , ... ,

$g(x)$,

$$U_d = \sum_{i=1}^N q_i u_i[x_i; d(x_i)], \quad i - \quad (\quad , \quad),$$

$$q_i = \frac{S_i}{S} \quad i - \quad , \quad S_i - \quad i -$$

$(\quad , \quad km^2)$, $S -$

X.

\bar{X} ,

$$U_{nd} \cdot \quad ,$$

N x_i

$$X = x_1, x_2, \dots, x_n, \quad :$$

$$U_{nd} = \sum_{i=1}^N q_i u[x_i; d_i(\bar{x})], \quad \bar{x} = \sum_{i=1}^N q_i x_i \cdot$$

$$\Delta U_1 = U_d - U_{nd}[d(\bar{x})] \quad (\quad -$$

(NDS);

(DDS);

(PDS). NDS

X

(\quad)

$g(x)$.

. DDS

$$U_{nd} = \int_{(x)} u[x, d(\bar{x})] g(x) dx \cdot$$

$$U_{nd}[d(x)]$$

DDS

$$x = a_0, \quad \bar{X},$$

(PDS).

“

”

X

$g(x)$.

$$\Delta U_1$$

$$\Delta U_2 = U_{nd}[d(a_0)] - U_{nd}[d(\bar{x})],$$

X.

$$\Delta U_1$$

$$\Delta U_2 \cdot$$

$$\gamma = \frac{\Delta U_2}{\Delta U_1}$$

[1].



$$\gamma, \Delta U_1, \Delta U_2$$

PDS

$$X, \Omega^{(1)}, \Omega^{(2)}, \dots, \Omega^{(n)}$$

“ ”

; PP – ; KP – ; EP – ; FP – ; FRP – ; PRP –

$$10^\circ$$

$$PP = \frac{\sum FAR}{g} \cdot \eta, \quad \sum FAR - ; \eta -$$

; g –

$$C_g -$$

$$q^{(n)},$$

q

N

X.

$$w^{(N)} = u_g^{(N)} - c_g q(N),$$

$$KP = \frac{E}{E_0} \cdot PP$$

$$KP = \frac{(W_H - W_K + Q)}{2,4 \cdot R} \cdot PP,$$

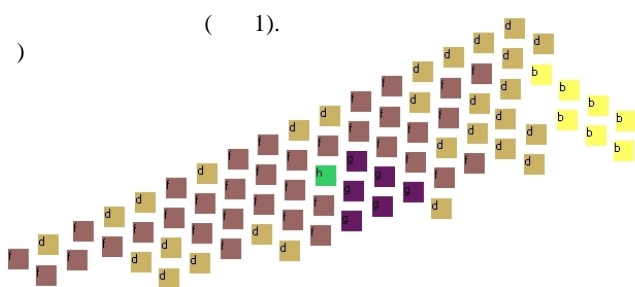
; E – ; E₀ – ; W_H – ; W_K –

$$N_0, \quad w^{(N_0)} = \max w^{(N)}$$

; Q – ; R – 10°

$$EP = B \cdot KP,$$

(1).



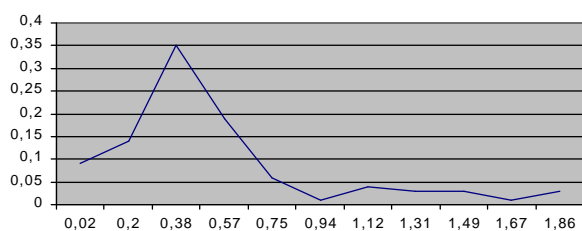
$$(B = a_0 + a_1 \cdot pH + a_2 \cdot H + a_3 \cdot P_2O_5 + a_4 \cdot K_2O, \quad pH - , H - , P_2O_5 - , K_2O -)$$

(B)

(FP)

$$\Delta P = EP - FP.$$

ΔP



1. ().

()

().



$$EP = FP \quad FP = FRP;$$

$$EP = FRP - \xi(FRP - FP) \quad FR < FRP;$$

$$EP = FRP + \xi(FP - FRP) \quad FP > FRP. \quad =1$$

$$(\Delta P = 0); \quad = 0$$

$$\left(\frac{\overline{FP}}{\overline{EP}} \right),$$

$$\left(\frac{\sigma_{FP}}{\sigma_{EP}} \right).$$

$$(PRP)$$

$$C_{\gamma},$$

$$C_T$$

$$FP,$$

$$U = \alpha \cdot C_{\gamma} \cdot FP - C_T \cdot PRP, \quad \alpha -$$

$$PRP \quad FP$$

$$PRP$$

$$(\overline{U} = C_{\lambda} \overline{EP} - C_T \cdot PRP), \quad PRP$$

$$\frac{\partial \overline{EP}}{\partial PRP} = \frac{1}{C_{\gamma}} \cdot \frac{\partial C}{\partial PRP} \cdot PRP.$$

$$a \quad b$$

$$\Phi(t) = \frac{1}{\sigma \sqrt{2\pi}} \int \exp\left(-\frac{(t-\mu)^2}{2\sigma^2}\right) dt, \quad \mu -$$

$$\Phi_{PRP} = \frac{1}{2} - \frac{b}{C_{\gamma} \cdot (1-\xi)}, \quad \Phi_{PRP} -$$

$$\frac{b}{C_{\gamma} \cdot (1-\xi)} < \frac{1}{2}$$

$$t_{FP}$$

$$\frac{b}{C_{\gamma} \cdot (1-\xi)} > \frac{1}{2}$$

$$t_{FP}$$

$$C_{PRP}.$$

$$\Phi(t_{PRP}) = \frac{1}{2} \cdot \frac{1-K}{1+K}, \quad K = \frac{b}{C_{\gamma}(1-\xi) - b},$$

$$t_{FP}$$

K	$\frac{1}{20}$	$\frac{1}{10}$	$\frac{1}{5}$	$\frac{1}{3}$	$\frac{1}{2}$	0	2	3	4	10	20
t_{FP}	1,67	1,34	0,97	0,63	0,43	0	-0,43	-0,67	-0,97	-1,34	-1,67

$$C_T \cdot PRP = m + l \cdot (PRP)^2, \quad m \quad l - \quad t_{FP}$$

$$\Phi(t_{PRP}) = \frac{1}{2} - \frac{2l \cdot \sigma_{FP}}{(1-\xi) \cdot C_{\gamma}} \left(t_{PRP} + \frac{\overline{FP}}{\sigma_{FP}} \right). \quad (FP),$$

$$\frac{l \cdot \sigma_{FP}}{(1-\xi) \cdot C_{\gamma}} < \frac{1}{4},$$

$$t_{FP}, \quad \frac{l \cdot \sigma_{FP}}{(1-\xi) \cdot C_{\gamma}} > \frac{1}{4}, \quad 1.$$

, 2007

TECHNOLOGICAL DIFFERENTIATION AND CHOICE OF A PLANNED PRODUCTIVITY LEVEL ON ACTUAL EFFICIENCY IN SYSTEMS OF PRECISE AGRICULTURE

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Summary. Variability of the factor of efficiency (x) can be presented by distribution function g (x), describing the factor as a random variable. Possibility of definition of planned productivity and allocation of contours on efficiency is being investigated.

Key words: precision agriculture, crop planning, differentiation.